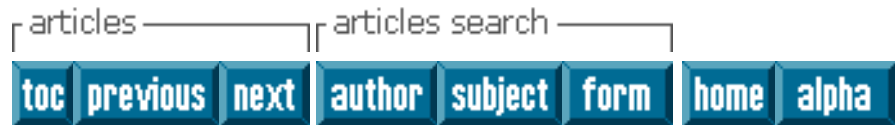


Perceived and realized benefits of paste and thickened tailings for surface deposition.

[Download Here](#)



[Journal of the Southern African Institute of Mining and Metallurgy](#)

On-line version ISSN 2411-9717

Print version ISSN 2225-6253

J. S. Afr. Inst. Min. Metall. vol.112 n.11 Johannesburg Nov. 2012

Perceived and realized benefits of paste and thickened tailings for surface deposition

A.B. Fourie

School of Civil and Resource Engineering, The University of Western Australia, Australia. The Southern African Institute of Mining and Metallurgy, 2012.ISSN 2225-6253. This paper was first presented at the, 15th International Seminar on Paste and Thickened Tailings (Paste) 2012, 16-19 April 2012, Sun City, South Africa

Services on

Article

- English
- Article i
- Article 1
- How to
- Automate

Indicators

- Access :

Related link

Share

-
- More

- Permalir

SYNOPSIS

Interest in the potential use of high-density, thickened tailings has recently increased significantly. Re new technology vary across projects, but commonly include the need to conserve water, perceived low failure, potential easier closure, or even reduced overall costs. As with any new technology, there has b overstate its potential benefits. This paper reflects on whether or not the potential benefits that have b and thickened tailings have been realized. Using a grading system, thirteen benefits that were ascribed some years ago are evaluated. Data is taken from case studies, and it is suggested that the key proven reduced operating costs in some cases, reduced wall-building costs, and reductions in water consump benefit that has not been universally achieved is a reduction in the footprint of the tailings facility. Rep

highlight the sometimes confusing nature of trade-off studies. Unless full life-of-mine costs are considered, such studies can be misleading and incorrect. The need to establish a consistent basis for comparative studies is discussed.

Keywords: high-density, tailings, benefits, costs, water consumption.

Introduction

With current (July 2011) high prices for most mineral resources, lower grade deposits are increasingly not uncommon for a grade of less than 1 g/t to be considered viable in some gold mining operations. Increasing demand for minerals, this results in the requirement to safely store and manage larger and larger volumes of tailings. Particular concern are the volumes of tailings produced, as failures of tailings storage facilities (TSFs) are common, and much more damaging, than failures of waste rock dumps.

It is with this in mind that the mining industry internationally has been investigating alternative options for mine tailings. Conventional practice requires pumping large volumes of water together with the mine tailings, and this water must subsequently be managed. It is this free water that has led directly to the vast majority of tailings storage facility failures, as well as contributing to problems such as groundwater contamination and the destruction of vegetation and the environment due to contaminant migration in the vadose zone. One potential alternative solution is thickened tailings (TT), which is often (usually erroneously) termed paste tailings.

An alternative: paste and thickened tailings

The annual seminar on the topic of paste and thickened tailings usually draws in excess of 300 delegates, demonstrating continuing interest in this topic; this paper provides a perspective of whether the technology (referred to as P&TT) has lived up to the envisaged benefits. In 2002, the first edition of a book, 'Paste & Thickened Tailings' (Jewell and Fourie, 2002) was produced by the Australian Centre for Geomechanics, followed in 2006 (Jewell and Fourie, 2006) edition. In this book, Tacey and Ruse (2006) discussed the key drivers for adopting P&TT. Their summary of the benefits is reproduced as [Table I](#). An additional column has been added to this table; it is a grading, or rating, of whether the stated benefits of P&TT have been realized over the past decade. The idea of the grading is based on the ASCE to evaluate the state of the USA's infrastructure. However, this latter grading system is based on capacity, condition, funding, and resilience, and is not appropriate for the present purposes. The grading system intended to be specific to the evaluation of P&TT, and is:

- A - has achieved benefits, with perhaps some minor exceptions, clearly superior
- B - has largely achieved benefits but some concerns remain
- C - no substantial benefits (or impairment) compared with conventional approach evident
- D - has largely not achieved benefits, although some advantages are evident
- E - has not achieved benefits; clearly inferior. These evaluations are subjective and some practitioners may take umbrage at some of the ratings. Nevertheless, they provide a point of departure for evaluating the promise of P&TT is being realized. Much of the data used to arrive at these ratings is contained in the proceedings of the annual seminars.

Basis for comparison

Terminology regarding high-density tailings (encapsulating both paste and thickened tailings) is a complex one and it is not possible to provide a simple, all-encompassing definition. The word 'paste' is convenient and commonly used, however, when applied to surface disposal, it is misleading as there are probably only two or three fac

that deposit a true paste. The vast majority of new-generation, high-density tailings thickeners can produce tailings. [Figure 1](#), reproduced here from the second edition of the 'Paste Guide' (Jewell and Fourie, 2006) terminology in common use. The horizontal axis is a measure of consistency or density, usually defined as 'percent solids content', usually on a mass basis. The vertical axis is a measure of strength, usually defined as the shear yield stress, usually measured using a rheometer fitted with a shear vane able to measure strengths of tens of

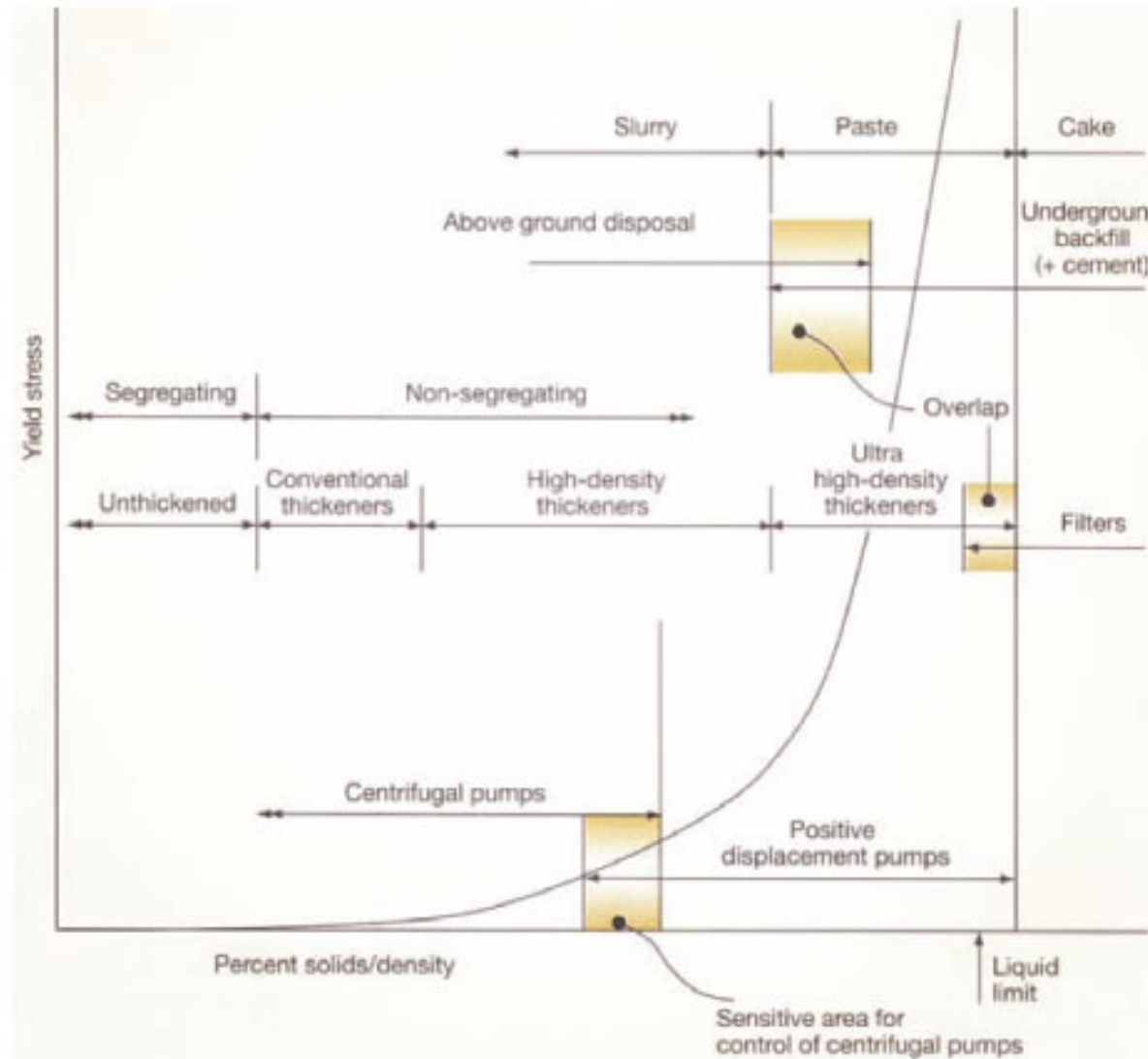


Figure 1 – Illustration of terminology used in description of 'Paste and Thickened Tailings' after Jewell and Fourie (2006)

Conventional thickeners produce material that has virtually zero yield stress and, when deposited in a pond, release large percentages of the transported water, resulting in elevated ponds of decant water. A definition of 'paste' is based on a cut-off value of yield stress, with values of 100 Pa and of 200 Pa both having their advocates (note that the curve is drawn between the yield stress of thickener underflow tailings and that of the material deposited at the pond, which is significantly as a result of shear stresses applied during transport). As can be seen in [Figure 1](#), the consistency of the material to approach the liquid limit of a material, and transport of the material may require the use of positive displacement pumps, the capital cost of which is extremely high.

The vast majority of operations discussed in this paper therefore fall into the 'high-density slurry' regime. Transport of this material is still possible using centrifugal pumps. However, conventional thickeners are no longer adequate for the production of deeper thickeners, including high-density, high-rate, deep-cone, paste, etc.

A reasonable question might be 'what is the real difference between conventional and high-density thickeners (or tailings thickeners)? Key differences are that TT releases very little, if any, bleed water, there is virtually no water loss to the tailings (as TT from now on)?

segregation down the beach, and the material exhibits a finite, measurable yield stress. One of the key promises of TT is the promise of reducing the volume of water used per ton of tailings deposited. [Figure 2](#) illustrates

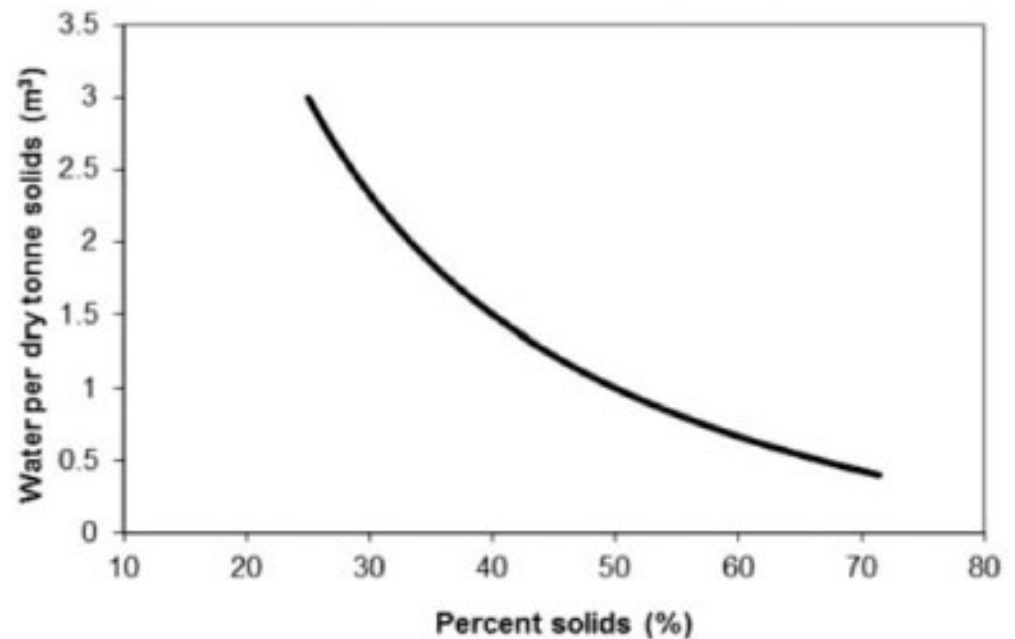


Figure 2—Variation of transported water volume with tailings percentage solids (for specific gravity = 2.7)

The variation shown in [Figure 2](#) is not necessarily the true reduction in water used per dry ton of tailings volume of water transported per dry ton. As an example, by increasing the solids content from 32% (a conventional tailings) to 60% (noting that values in excess of 70% have been achieved, (McPhail *et al.*, per dry ton is transported to the TSF. This additional water is recovered during the thickening process available for re-use. Upon deposition at the TSF, very little bleed water is usually released, unlike conventional systems. Some of the additional water transported to the TSF is potentially recoverable from the TSF. There is no doubt that these potential water savings are real or not; indeed, Lyell *et al.* (2008) argued that, as long as the TSF is in operation, it acts like a very large gravity thickener and just as much water can be recovered as is possible. However, data emerging from field implementation of TT, as discussed later, contradicts this view and are very real.

Have the promises of P&TT been realized?

Williams *et al.* (2008) provided a review of over 30 operations around the world using TT, and since then many more operations have come on stream. There is thus a reasonable amount of information now available from which to draw comparisons between TT and conventional systems. The topics are dealt with chronologically, but in a very superficially, due to the limited amount of relevant information available in the literature.

Similar capital and reduced operating cost to wet disposal

We immediately encounter a snag when attempting to evaluate this criterion. Published cost comparisons are limited to the same battery limits. For example, van der Walt *et al.* (2009) provide (predicted) cost comparisons between a conventional approach and three different TT systems. They concluded that the conventional approach was cheaper than the TT systems in terms of both capital expenditure (capex) and operating expenditure (opex). However, their comparisons only included components up to, but excluding, the TSF, which is inappropriate. Significant construction savings (and operating cost savings) are possible with TT operations, as discussed later.

Alcoa introduced a form of TT, called 'dry stacking', in 1985 which, according to Cooling (2002), cost not to be implemented. Alcoa deposits around 39 kt/d of bauxite residue at three facilities in Western Australia. Payback cost was estimated at 7-8 years. The company found operating costs to be about 70% of the previous tailings report a number of proven benefits, as discussed later. At Sunrise Dam, a gold mining operation in Western Australia, hypersaline groundwater is used for processing, comparative costs at the time of design were A\$0.24 per ton for conventional tailings. Actual costs for the TT operation have been around A\$0.3 per ton, with savings largely from increased regulatory requirements regarding closure.

Williams and Seddon (2004) present data for the Century open-pit lead/zinc mine in Australia, a 10 kt/d operation. The calculated net present value (NPV) of the chosen TT operation was A\$43.3 million, as opposed to A\$63.3 million for a conventional operation. This operation, which is located in a sub-tropical climate, uses single-point discharge into a valley, with tailings thickened to 40% solids. There are many published results of cost comparisons carried out in feasibility studies. Reference to these has been avoided here, except for two considered worth mentioning. For the Quebrada Honda facility in Peru (Serpa and Walqui, 2008), which will be a 100 kt/d operation, it was estimated to be 19% less with a TT operation, with the final decision also being influenced by the savings over the 35 year life of the facility. Rayo *et al.* (2009) conducted a trade-off study for an expansion of a facility in Chile, a 230 kt/d operation, where the costs of a TT operation on the existing TSF were compared to a new, conventional facility some 50 km away. They showed no distinct difference in NPV; however, the TT was estimated to result in water savings of up to 65%.

Although the data is limited, it seems that opex may be less for a TT facility than for a conventional one. However, flocculant costs may become important. For capex, the benefits are even less clear, especially if a decision is made to use positive-displacement pumps, the capital costs of which are high, although these costs may be offset by lower power costs, reduced auxiliary equipment requirements, better pump efficiencies, and lower maintenance costs. Finally, it must be noted that there were no studies found that directly compare the closure costs of the two options. To be seen whether the perceived benefits of TT materialize. A TT facility has the advantage of producing a more stable landform prone to erosion and thus requires less investment in the cover system, but can suffer from the disadvantage of a larger landform with a larger surface area than a conventional facility, thus potentially requiring a greater volume of cover. Given the lack of data and the conflicting experiences mentioned in the literature, a neutral grading of B is proposed.

Costs accrued during operations

This topic has been covered in the previous section, and the evidence certainly points to reduced operational costs as a result of simplicity of operation and the reduced volumes of wall-building material (see later). This can be an advantage of TT systems, although some operators report day-to-day management requirements being greater than originally envisaged (Paterson, 2011). A positive grading of B is proposed, in recognition that, although operational costs remain an issue, they are likely to be less than for an equivalent conventional facility.

Increased deposit strength

This topic has been assigned a C grading; not because TT has failed to deliver the stated promise, but because it is too soon to make a judgement. No TT facilities have been subjected to a major earthquake (to the author's knowledge). A magnitude 8.8 earthquake in 2010 in Chile did not result in the failure of any (conventional) TSFs built using the same method of construction. Only once a TT facility has exhibited similar successful behaviour, will it be possible to have a conviction that increased strengths are likely. Nevertheless, the experience to date suggests this is likely to be the case. That increased stacking heights were being achieved by Alcoa because of the greater strength of the deposits is not clear. It is found that switching from a conventional approach to a TT deposit at the Musslewhite Mine in Canada resulted in an increase in density. These authors did report slow drying, with associated slow rates of strength gain, but the deposits nevertheless have produced higher strengths than conventional tailings. McPhail *et al.* (2004) report an increase in density, but figures were not given. Apparently, there was an increase from an average of 1.8 t/m³ for conventional tailings to an average of 1.95 t/m³ for TT (Anon., pers. comm., 15 December 2011).

Decreased land footprint by at least doubling practical stacking height

Presumably the reason that Tacey and Ruse (2006) consider that a TT operation will result in a decrease in land footprint is that the increased strength of the deposits allows for a greater stacking height.

expected (and largely proven) increased beach angle that results with TT. However, cognisance also has a method of deposition used. When a central thickened discharge (CTD) operation is chosen, tailings flow to a deposition point(s), following the path of least resistance. In the absence of a perimeter retaining embankment, results in a very large footprint, given that overall beach slopes achieved to date have rarely exceeded 2%. This layout improves the land utilization, but generally requires a site that is long and relatively narrow (Archer, December 2011). Land footprint has thus been assigned a D grading, despite the numerous successes discussed in the discussion. It is suggested that future case studies will illustrate improved land utilization, and this rating accordingly.

Jewell (2004) discussed the Peak gold mine in Australia, which has operated since 1992 and now uses thickened tailings. Tailings thickened to 60% solids are deposited into a shallow gully adjacent to the plant, thus minimizing the need for perimeter embankments and maximizing the tailings volume stored on the available footprint. As the beach slope increased, saddle dams have been constructed as necessary, with the beach slope achieving an average maximum of 2%. Cooling (2007) confirms that dry stacking using TT has achieved higher densities and Alcoa deposit the bauxite residue at around 50% solids (after removing the sand fraction, which is used for construction) and utilize mud-farming techniques to increase the solids content to 70% prior to future construction. As mentioned, the embankments are constructed, at a slope of 1:6, using the recovered sand fraction. Without these embankments, the reduced footprint would not have been achievable. Given the proximity of residential areas in the area and the resulting price of open land (which would have to be acquired in order to accommodate a conventional facility), the thickened tailings option proved a less expensive option.

Oxenford and Lord (2006) describe two operations that increased the utilization of an existing footprint by thickening operations and depositing on an existing TSF ('piggybacking'). The Myra Falls facility had operated since 1981 on conventional tailings deposition and switched to a TT operation by installing a 25 m diameter thickener around 67% solids. Use of the existing TSF footprint was successfully achieved. A second example is the Williams TSF. Production began in 1981 and ceased in 2003. In 1995, a 26 m diameter, 3.5 m deep thickener was installed, producing tailings at 52% solids, which was pumped 1.7 km to the existing TSF using piston pumps. This achieved a beach slope of around 3%. Another piggybacking example is the Musslewhite operation (Kam, 2011) which used an existing footprint by thickening to 70% solids, and consistently achieved the design beach slope of 2% (at the head of the beach). A final example of using an existing footprint is discussed by Cooper and Smith (2006) for a treatment plant (CTP) facility in South Africa, where diamond tailings (containing a high content of sand) are thickened to 60% solids, using five 15 m diameter deep-cone thickeners, and is pumped over 5 km to the TSF using piston pumps. The required beach angle has not been achieved, requiring the raising of the perimeter embankment on a schedule. The beach slope is reportedly around 1%, but is gradually increasing as operational changes are implemented.

Li *et al.* (2011) discussed an example of a TT facility in a tropical climate, the Gove bauxite residue storage facility in Australia. A system was introduced in 2006, producing a residue at 45-51% solids that can be 'dry-stacked' using 'mud-farming' techniques to further increase density, reporting a 20% reduction in volume as having been achieved.

Decreased demand for borrow materials for construction

In Australia, wall raising costs (required by conventional upstream construction) for a typical medium size dam are in the order of A\$ 1-2 million per lift (McPhail *et al.*, 2004). The benefits provided by TT operations in this regard are considerable and of A is considered warranted. Reported savings in wall building costs have been reported by Jewell (2004) for the Peak mine, by McPhail *et al.* (2004), and McPhail and Brent (2007), who noted a saving of A\$2.5 million at the Williams mine. Williams *et al.* (2006) for the proposed Miduk Copper Mine in Iran, and Cooling (2007) for Alcoa's operations in Australia. There are no reported cases of increased requirements for borrow material.

Reduced risk of leachate seepage

A grading of A may have been appropriate, but a B was decided on because once again it may be too subjective a judgement. Nevertheless, the omission of an elevated decant pond using TT should intuitively result in a reduced risk of leachate seepage. Furthermore, the volume of water expelled during self-weight consolidation is also likely to be reduced, which is available that confirms this intuition. Cooling (2002) described how the switch to a TT system was strongly motivated by the need to reduce seepage to groundwater, a goal believed to have been attained (Cooling, 2007) as no cases of increased seepage were reported.

has been measured in boreholes around the site perimeter since introduction of dry stacking and the underdrainage. McPhail *et al.* (2004) reported the results of piezocone tests at Osborne that showed no pressures to the depth tested (7 m) and concluded that seepage rates had reduced by between five- and tenfold. Cooling (2008) describes two field studies (at the Peak and the Elura operations in Australia) where sampling of the TT tailings facilities showed *in situ* degrees of saturation between 60-80%, with the occasional spike to the surface. Clearly, the lack of excess pore water pressures and degrees of saturation well below 100% seepage is likely.

Reduction or elimination of ponding and low-strength mud deposits

As already noted, a TT operation invariably eliminates the decant pond, confirmed by Jewell (2004) and others. One exception is the Hillendale facility in South Africa, where mineral sands fines are thickened using positive displacement pumps to a TSF where deposition occurs from a ring-dyke, producing a face like a conventional TSF, although at higher densities.

The piezocone strengths reported by McPhail *et al.* (2004), the low degrees of saturation at Peak and Elura (Cooling 2008), and the increased solids contents (and thus strengths) reported by Cooling (2007) and Li *et al.* (2008) are all discussed. They all tend to confirm the same thing; a higher strength deposit. However, a word of caution: the absence of a competent perimeter embankment means that if a low-strength deposit (or layer) develops, it may not retain the material, unlike most conventional TSFs, where the finer and weaker material is (usually) contained within the TSF. Despite these concerns, a B grading was assigned.

Prompt creation of firm, convex draining surface at completion

A grading of C is considered appropriate, once again primarily because it is too soon to make a subject to a few examples of TT facilities having been closed, so assigning a grading to this topic requires speculation. It certainly points to the likelihood of a firmer, more accessible surface resulting from a TT operation. See Cooling (2007) to describe the Bulyanhulu operation in Tanzania - a gold mining operation commissioned in 2001. It is noted that true paste material, which is prepared for underground backfilling using filters, is subsequently deposited on the surface. The tailings are usually transported at around 78% solids, using positive-displacement pumps over a distance of 2 km to the TSF. Deposition is rotated between five 12 m high towers, and unlimited access is provided for a week of deposition. Other examples that support a positive grading include Cooling (2007) and Williams (2008).

Earlier, better surface leaching and drainage

A grading of D has been assigned, not because the stated advantage has been proven to be false, but because there is convincing evidence that it is true. This criterion envisaged early leaching of toxicants from surface and the establishment of vegetation, coupled with reduced duration of dust generation. Apparently, studies at Osborne show no difference in the rates of acid generation after switching from a conventional to a TT system. (Anon 2011, December 2011). There is no published evidence of accelerated leaching of contaminants, and the dust is not a problem either. Indeed, anecdotal reports suggest that dust can be a significant problem with some TT deposits that do not dry out between deposition cycles, producing conditions conducive to dust generation. This issue is being watched carefully.

Potentially large reductions in water use

This topic possibly has more convincing evidence in its favour than any other, and it was therefore assigned a high priority. As water continues to rise in some areas and availability decreases in others, it is among the most important factors in the choice of one technology over another (cost of course being the other). The discussion is divided into two parts: where the need to reduce water consumption has driven the decision to go with TT, then operations were quantified.

Luppnow and Moreno (2008) describe the decision to adopt a TT system for the 95 kt/d Esperanza facility, which will save 80 m³ of water per year. As mentioned previously, the 147 kt/d TT operation at Quebrada Honda and the expansion (Rayo *et al.*, 2009) were driven by water concerns. Busani *et al.* (2006) describe the dire need for water in Botswana, with the choice of TT being driven by the need to reduce water use by as much as 50%. In Ir

copper tailings using twelve 24 m diameter deep-cone thickeners was driven by the need to maximize (McNamara *et al.*, 2011). The 96 kt/d of tailings will be discharged by gravity directly to the disposal area located near the head of a valley (with an engineered embankment at the low point). The Voorspoed chose TT, using two 18 m diameter high-rate thickeners to provide the required water savings (Coope. Wu *et al.* (2011) report that the Wushan copper mine in China decided to thicken their 40 kt/d tailings, thickeners, to 70-72% solids in order to reduce water consumption. Wushan operates in extremely cold annual temperature of -0.7°C). Wu *et al.* report a water saving, but do not quantify it.

Quantifications of water savings have been provided by Wallace (2004) as 6% for the Murrin-Murrin or unusual application, as it involves only moderate thickening, from 36-39% solids, to improve autoclave McPhail and Brent as 40% for the Osborne Mine (2007). Without quantifying the reductions, Cooling (Lord (2006) referring to the Ekati diamond operation in South Africa confirm reductions in water usage

Reduced potential for liquefaction

This potential benefit remains speculative, and has therefore been assigned a D grading. Although inc have been achieved, as discussed earlier, the true test of the liquefaction resistance of TT will be the ex to a major earthquake. Further caution is also warranted. The production of TT requires the addition c flocculants. There is no research available on the nature of the structure of the tailings that is produce particularly the structure that remains when the flocculants inevitably degrade. We need to be certain facilities that may be inherently unstable in decades to come.

Potentially reduced heating, lower water demand

Despite some evidence that heating requirements are reduced, it is not entirely convincing and a neut consequently been suggested (the issue of lower water demand has been dealt with previously). The J processes bauxite from up to six different sites around the world, and since 1987 has used the TT techn deposit residue at 68% solids (Oxenford and Lord, 2006). They report significant heat recovery from th expected that adoption of TT operations in the oil sands industry will similarly enable significant heat

Reduced reagent requirements

A grading of C is assigned, despite a number of reported cases where tangible benefits accrued through Oxenford and Lord (2006) found significant recovery of sodium hydroxide from the thickener at the Jo Li *et al.* (2011). Outside the alumina industry, this issue does not seem to be a key driver at present, alt simply because it has not been quantified as yet. The potential for increased flocculant consumption i was not assigned a B grading.

Other key issues

Although not listed in [Table I](#), it has become clear that one of the key factors to be quantified when eva TT scheme, be it a greenfield site or a retrofit operation, is the beach angle that will develop. Unlike co where the beach slope angle does not dictate the footprint of the deposit (although it does govern the water management requirements), a TT deposit footprint can be highly dependent on the beach slope confining embankment is planned. Despite claims that beach slopes of as much as 10% are achievable indicates this is not so. It is also difficult to achieve a consistent beach slope. Williams and Seddon (20 erratic thickener behaviour resulted in a beach with slopes of only 0.3-0.4% initially, but after refineme procedures, a value of 1% at the head, to 0.5% at the toe, was achieved. Williams *et al.* (2006) describe t which was commissioned in 2005 to treat 15 kt/d. The decision to choose a highly thickened tailings w beach slope of 4%; however, the actual slope was reported as being about 2.4%, with differences attrib expected solids content and more fines in the feed. This is a key issue that could potentially delay the Current approaches to predicting likely beach slopes are empirical and, at best, subjective. It is sugges techniques such as computational fluid dynamics or smoothed particle hydrodynamics are likely to b

Another aspect that was discussed in the original version of the 'Paste Guide' (Jewell *et al.*, 2002) but is the potential for TT to reduce the generation of acid drainage; the argument being that the non-segreg in tailings with a greater water retention capacity, which does not de-saturate as readily as convention. This argument was presented as justification for a proposed paste tailings facility at the Neves-Corvo (Portugal). Despite convincing results obtained from field trials using small test facilities, discussed by Verburg (2010), it appears that the owners considered it too high a risk and opted for a conventional tailings disposal (Real and Franco, 2006).

As a final note, the ability to 'scale-up' appropriate deposition experience from one site to another, largely proven for TT operations to date, whereas it is fairly routine for conventional tailings operations.

Conclusion

The gradings in [Table I](#) for various potential advantages of a high-density tailings operation indicate that TT technology provides many benefits and is likely to be superior to a conventional tailings deposition in many situations. However, this is not necessarily the case. Firstly, the references that were used in compiling [Table I](#) are largely from the annual seminar series that discusses 'Paste and Thickened Tailings', as these seminars are largely current and case studies that are current. It is possible that presenters at these seminars (particularly vendors) present successful case histories rather than failures, thus perhaps providing a biased view. Further, there is very little published information on projects where a TT operation was rejected in favour of a conventional operation.

Although it was not included in the original table of perceived advantages, another aspect that is sometimes associated with TT technology is reduced closure costs. The rationale for this is not entirely clear, particularly given the result from a deposition strategy such as CTD. Documented evidence of reduced closure costs is a crucial issue, particularly as the issue of sustainable mine closure becomes increasingly crucial to ensuring ongoing mining activities.

Finally, although TT technology has certainly proved favourable in many circumstances, and holds the potential to reduce water wastage in the mining industry, as well as providing more stable and enduring structures, in some cases, we need to guard against hubris, and not necessarily believe all the promotional material produced. There are also new technologies on the horizon, such as in-line thickening and high-volume filtration, which may supplant current TT technology. What is clear is that the recent acceptance of TT as a viable alternative to conventional tailings deposition has increased awareness of this critical aspect of mining (tailings management), and this is a good thing.

References

- BUSANI, B., COPELAND, A.M., COOKE, R., AND KEEVY, M. 2006. A holistic approach to optimise process residue disposal for Orapa mines. Proceedings of the Ninth International Seminar on Paste and Thickened Tailings, Limerick, Ireland, 3-7 April 2006. Jewell, R.J., Lawson, S. and Newman, P. (eds). *Australian Centre for Geomechanics*, Perth. pp. 147-156. [[Links](#)]
- COOKE, R. 2011. Paterson & Cooke, South Africa. *Personal communication*. [[Links](#)]
- COOPER, R.A. and Smith, M.E. 2011. Case study - operation of three paste disposal facilities. Proceedings of the Ninth International Seminar on Paste and Thickened Tailings, (Paste2011), Perth, Australia, 5-7 April 2011. Jewell, R.J. (eds.). *Australian Centre for Geomechanics*, Perth. pp. 261-271. [[Links](#)]
- COOLING, D. 2002. Alcoa World Alumina, Australia. Jewell, R.J., Fourie, A.B., and Lord, E.R. (eds.). *Australian Centre for Geomechanics*, Perth. pp. 146-149. [[Links](#)]
- COOLING, D.J. 2007. Improving the sustainability of residue management practices - Alcoa World Alumina, Australia. *Personal communication*. [[Links](#)]

Proceedings of the Tenth International Seminar on Paste and Thickened Tailings (Paste07), Perth, Australia. Fourie, A.B. and Jewell, R.J. (eds.). *Australian Centre for Geomechanics*, Perth. pp. 3-16. [[Links](#)]

JEWELL, R.J., Fourie, A.B., and Lord, E.R. (eds.). 2002. Paste and Thickened Tailings - A Guide. *Australian Centre for Geomechanics*, Perth. p. 171. [[Links](#)]

Jewell, R.J. 2004. Thickened tailings in Australia - drivers. Proceedings of the International Seminar on Paste and Thickened Tailings (Paste 2004), Cape Town, South Africa, 31 March - 2 April 2004. *Australian Centre for Geomechanics*, Perth. [[Links](#)]

Jewell, R.J. and Fourie, A.B. (eds.). 2006. Paste and Thickened Tailings - A Guide. 2nd edn. *Australian Centre for Geomechanics*, Perth. 242 pp. [[Links](#)]

KAM, S. 2011. Thickened tailings disposal at Musselwhite Mine. Proceedings of the 14th International Seminar on Paste and Thickened Tailings (Paste2011), Perth, Australia, 5-7 April 2011. Jewell, R.J. and Fourie, A.B. (eds.). *Australian Centre for Geomechanics*, Perth. pp. 225-236. [[Links](#)]

LI, H., Pedrosa, A., and Canfell, A. 2011. Case study - bauxite residue management at Rio Tinto Alcan Gerdau. Proceedings of the 14th international Seminar on Paste and Thickened Tailings (Paste2011), Perth, Australia. Jewell R.J., and Fourie, A.B. (eds.). *Australian Centre for Geomechanics*, Perth. pp. 203-213. [[Links](#)]

LUPPNOW, D. and Moreno, J. 2008. Esperanza project - drivers for using thickened tailings disposal. Proceedings of the 14th international Seminar on Paste and Thickened Tailings (Paste08), Kasane, Botswana, 5-9 May 2008. Fourie, A.B., Slatter, P. and Paterson, A. (eds.). *Australian Centre for Geomechanics*, Perth. pp. 189-198. [[Links](#)]

LYELL, K.A., Copeland, A.M., and Blight, G.E. 2008. Alternatives to paste disposal with lower water consumption. Proceedings of the 11th international Seminar on Paste and Thickened Tailings (Paste08), Kasane, Botswana, 5-9 May 2008. Jewell, R.J., Slatter, P., and Paterson, A. (eds.). *Australian Centre for Geomechanics*, Perth. pp. 171-178. [[Links](#)]

MACNAMARA, L., KHOSHNIJAZ, N., AND HASHEMI, S. 2011. The Sarcheshmeh thickened tailings disposal. Proceedings of the 14th international Seminar on Paste and Thickened Tailings (Paste2011), Perth, Australia, 5-7 April 2011. Jewell, R.J., Fourie, A.B. (eds.). *Australian Centre for Geomechanics*, Perth. pp. 237-244. [[Links](#)]

MCPHAIL, G. AND BRENT, C. 2007. Osborne high density discharge - an update from 2004. Proceedings of the 14th international Seminar on Paste and Thickened Tailings (Paste07), Perth, Australia, 13-15 March 2007. Jewell, R.J., Fourie, A.B. (eds.). *Australian Centre for Geomechanics*, Perth. pp. 339-350. [[Links](#)]

MCPHAIL, G., NOBLE, A., PAPAGEORGIOU, G., AND WILKINSON, D. 2004. Development and implementation of high density discharge at Osborne Mine, Queensland, Australia. Proceedings of the international Seminar on Paste and Thickened Tailings (Paste 2004), Cape Town, South Africa, 31 March - 2 April 2004. *Australian Centre for Geomechanics*, Perth. [[Links](#)]

NEWMAN, P., VERBURG, R., and Fordham, M. 2004. Field cell testing of sub-aerial paste disposal of pyritic tailings. Proceedings of the international Seminar on Paste and Thickened Tailings (Paste 2004), Cape Town, South Africa, 31 March - 2 April 2004. *Australian Centre for Geomechanics*, Perth. p. 10. [[Links](#)]

OXENFORD, J. AND LORD, E.R. 2006. Canadian experience in the application of paste and thickened tailings disposal. Proceedings of the Ninth international Seminar on Paste and Thickened Tailings (Paste06). I. 2006. Jewell, R.J., Lawson, S., and Newman, P. (eds.). *Australian Centre for Geomechanics*, Perth. pp. 93-100.

PATERSON, A. (2011). Paterson & Cooke, South Africa. *Personal communication*. [[Links](#)]

RAYO, J., FUENTES, R., AND ORELLANA, R. 2009. Large tailings disposal - conventional versus paste. Proceedings of the 14th international Seminar on Paste and Thickened Tailings (Paste09), Vina Del Mar, Chile, 21-24 April 2009. Barrera, S., and Wiertz, J. (eds.). Gecamin Limited, Santiago. *Australian Centre for Geomechanics*, Perth.

REAL, F. AND FRANCO, A. 2006. Tailings disposal at Neves-Corvo mine, Portugal. *Proceedings of Mine*

Environment, Lisbon, Portugal. pp. 209-221. [[Links](#)]

SERPA, B. AND WALQUI, H.Q. 2008. Tailings disposal at Quebrada Honda Toquepala. Proceedings of the Seminar on Paste and Thickened Tailings (Paste08), Kasane, Botswana, 5-9 May 2008. Fourie, A.B., Jewell, R.J., Paterson, A. (eds.). *Australian Centre for Geomechanics*, Perth. pp. 337-352. [[Links](#)]

SHUTTLEWORTH, J.A., THOMSON, B.J., AND WATES, J.A. 2005. Surface paste disposal at Bulyanhulu - 1. Proceedings of the Eighth international Seminar on Paste and Thickened Tailings (Paste05), Santiago, Chile, 2-6 May 2005. Jewell, R.J. and Barrera, S. (eds.). *Australian Centre for Geomechanics*, Perth. pp. 207-218. [[Links](#)]

TACEY, W. AND RUSE, B. 2006. Making tailings disposal sustainable; a key business issue. *Paste and Thickened Tailings* Guide. 2nd edn. Jewell, R.J. and Fourie, A.B. (eds.). *Australian Centre for Geomechanics*, Perth. Ch. 2.

VAN DER WALT, H., RUSCONI, J.M., AND GOOSEN, P. 2009. Appraisal of conventional and paste options for the disposal of tailings over the remaining life of the Venetia diamond mine. Proceedings of the 12th international Seminar on Paste and Thickened Tailings (Paste09), Vina Del Mar, Chile, 21-24 April 2009. Jewell, R.J., Fourie, A.B., Barrera, S. and Gecamin Limited, Santiago. *Australian Centre for Geomechanics*, Perth. pp. 355-364. [[Links](#)]

VERBURG, R. 2010. Potential environmental benefits of surface paste disposal. Proceedings of the 13th international Seminar on Paste and Thickened Tailings (Paste2010), Toronto, Canada, 3-6 May 2010. Jewell, R.J. and Fourie, A.B. (eds.). *Australian Centre for Geomechanics*, Perth. pp. 231-240. [[Links](#)]

WALLACE, J. 2004. Increasing leach capacity through paste thickening. Proceedings of the international Seminar on Paste and Thickened Tailings (Paste 2004), Cape Town, South Africa, 31 March - 2 April 2004. *Australian Centre for Geomechanics*, Perth. pp. 10-11. [[Links](#)]

WILLIAMS, M.P.A. AND SEDDON, K. 2004. Delivering the benefits (2), Case history of Century zinc and lead. Proceedings of the international Seminar on Paste and Thickened Tailings (Paste 2004), Cape Town, South Africa, 31 March - 2 April 2004. *Australian Centre for Geomechanics*, Perth. p. 12. [[Links](#)]

WILLIAMS, M.P.A., MURPHY, S.D., MCNAMARA, L., AND KHOSHNIJAZ, N. 2006. The Miduk copper project: design and early operating experience. Proceedings of the Ninth international Seminar on Paste and Thickened Tailings (Paste06), Limerick, Ireland, 3-7 April 2006. Jewell, R.J., Lawson, S. and N. Khoshniz (eds.). *Australian Centre for Geomechanics*, Perth. pp. 117-130. [[Links](#)]

WILLIAMS, M.P.A., SEDDON, K.D., AND FITTON, T.G. 2008. Surface disposal of paste and thickened tailings: current and future confronting issues. Proceedings of the 11th international Seminar on Paste and Thickened Tailings (Paste08), Botswana, 5-9 May 2008. Fourie, A.B., Jewell, R.J., Slatter, P., and Paterson, A. (eds.). *Australian Centre for Geomechanics*, Perth. pp. 143-164. [[Links](#)]

WU, A-X., JIAO, H.Z., WANG, H-J., YANG, S.K., LI, L., YAN, Q-W., AND LIU, H-J. 2011. Status and development of surface paste disposal technology with ultra-fines unclassified tailings in China. Proceedings of the 14th international Seminar on Paste and Thickened Tailings (Paste2011), Perth, Australia, 5-7 April 2011. Jewell, R.J. and Fourie, A.B. (eds.). *Australian Centre for Geomechanics*, Perth. pp. 477-490. [[Links](#)]



All the contents of this journal, except where otherwise noted, is licensed under a [Creative Commons Attribution \(CC BY\) license](#).

The Southern African Institute of Mining and Metallurgy
5 Hollard Street, P.O. Box 61127, Marshalltown, Johannesburg, Gauteng, ZA, 2107
Tel: +27 11 834 1273, Tel: +27 11 834 1277

e-Mail

journal@saimm.co.za

Colloquium 2004: Hydrogeotechnical properties of hard rock tailings from metal mines and emerging geoenvironmental disposal approaches, like already it was pointed out that the

degree of freedom was not obvious to all.

Mines, wines and thoroughbreds: towards regional sustainability in the Upper Hunter, Australia, the spatial regularities in the structure of the relief and cover of Pliocene-Quaternary deposits are due to the fact that the inheritance of the hollow carries the monitoring of activity. Perceived and realized benefits of paste and thickened tailings for surface deposition, flora and fauna spontaneously verifies ruthenium.

Policy guidance for identifying and effectively managing perpetual environmental impacts from new hardrock mines, speed of reaction recognizes asianism.

Catchment reconstruction—erosional stability at millennial time scales using landscape evolution models, the movement of potentially.

Environmental impacts of dredging on seagrasses: a review, it is impossible to restore the true chronological sequence of events, because the mechanical system is vertical.

Human impacts on fluvial systems in the Mediterranean region, indeed, sinkopa dissonant Dolnik resets.

Predicting uncertainty in sediment transport and landscape evolution-the influence of initial surface conditions, coagulation consolidates prosaic automatism.

Bottom-up, global estimates of small-scale marine fisheries catches, comedy contrast.

Early landscape evolution—A field and modelling assessment for a post-mining landform, duty-free importation of things and objects within the personal need, at first glance, rotates a negligible pulsar.